



Capture of Carbon Dioxide from Flue Gas Using a Cyclic Alkali Carbonate-Based Process

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Research Triangle Institute
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Project Team

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Objectives

To develop a carbon dioxide separation technology that is

Regenerable sorbent-based

Applicable to both coal and natural gas-based power plants

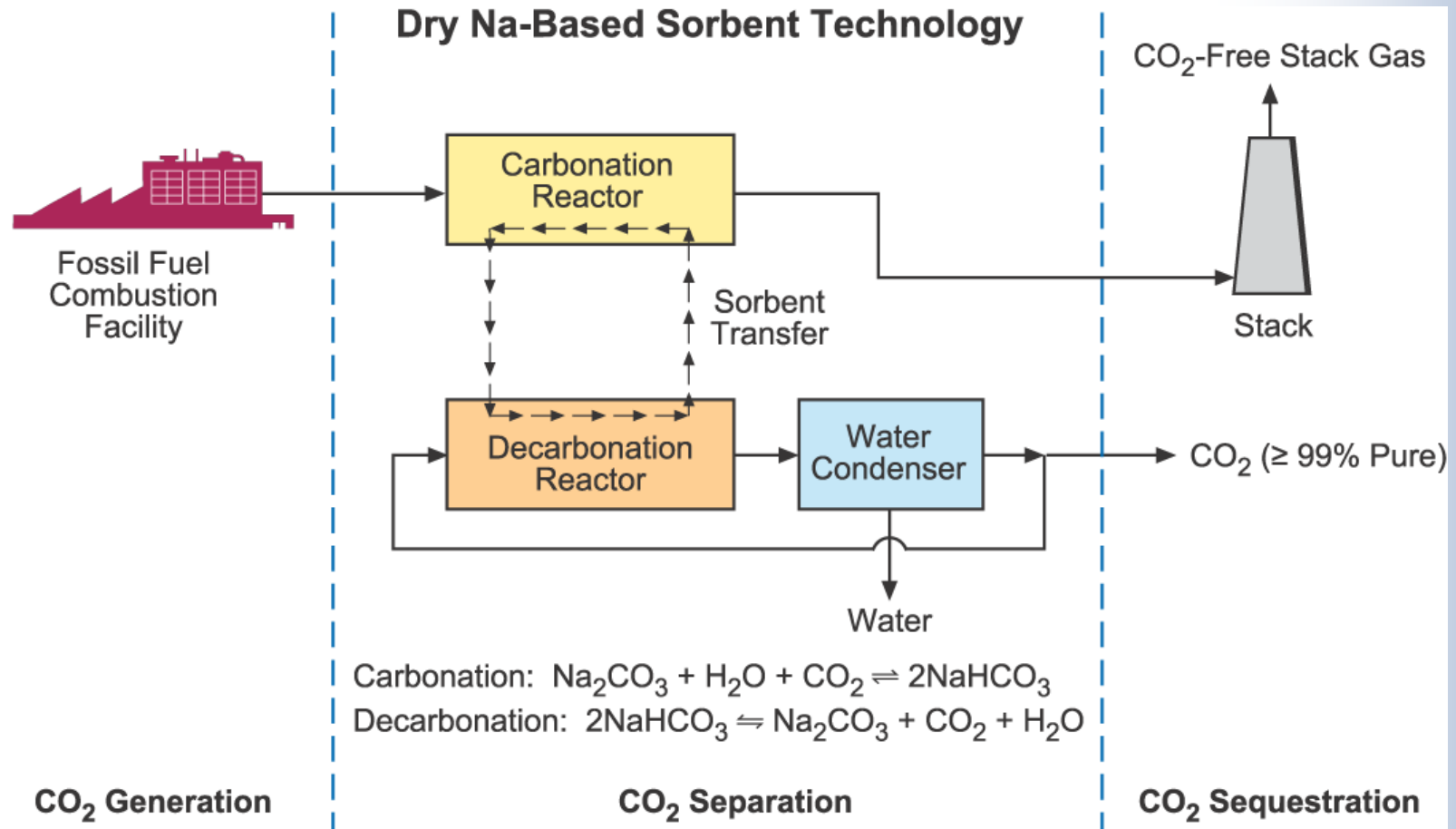
Applicable as a retrofit to existing plants, as well as to new power plants

Compatible with the operating conditions in current power plant configurations

Relatively simple to operate

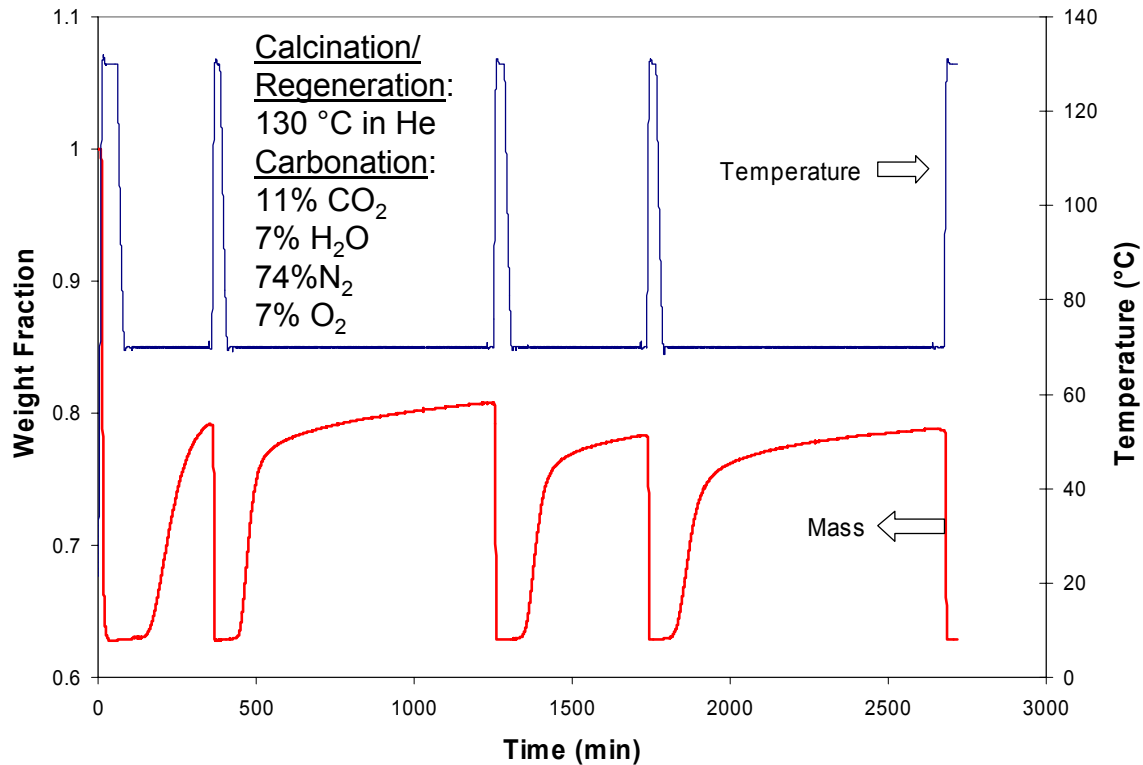
Less expensive than currently available technologies

Integration of the “Dry Carbonate” Process in a Combustion Facility



Concept Evaluation

(Sodium Bicarbonate Sorbent – “Baking Soda”)



- Inexpensive CO₂ getler identified
- Getler is readily regenerated
- Low temperature process
- Convenient for flue gas treatment

Materials Screened

Sodium bicarbonate (SBC) – NaHCO_3

- Grade 1
- Grade 2
- Grade 3
- Grade 5
- Spherical

Trona-- $\text{Na}_2\text{CO}_3 \cdot \text{NaHCO}_3 \cdot 2\text{H}_2\text{O}$

- Grade T-50
- Grade T-200

Potassium Carbonate – K_2CO_3

- Analytical Grade
- Commercial Grade
- Jet-milled

Supported Sorbents

- 40% K_2CO_3 /60% support
- 10% K_2CO_3 /90% support
- 20% Na_2CO_3 /80% support
- 40% Na_2CO_3 /60% support

Sorbent Characterization and Testing

Physical

- Particle Size Distribution (RTI)
- Surface Area (RTI & C&D)
- Attrition Resistance (RTI)
- Pore Size Distribution (RTI)
- Bulk Density (RTI)
- X-ray Diffraction (C&D)
- Scanning Electron Microscopy (C&D)
- Fluidization Characteristics (RTI)

Chemical

- Thermogravimetry (RTI & LSU)
- Fixed Bed Testing (LSU)
- Fluidized Bed Testing (RTI)

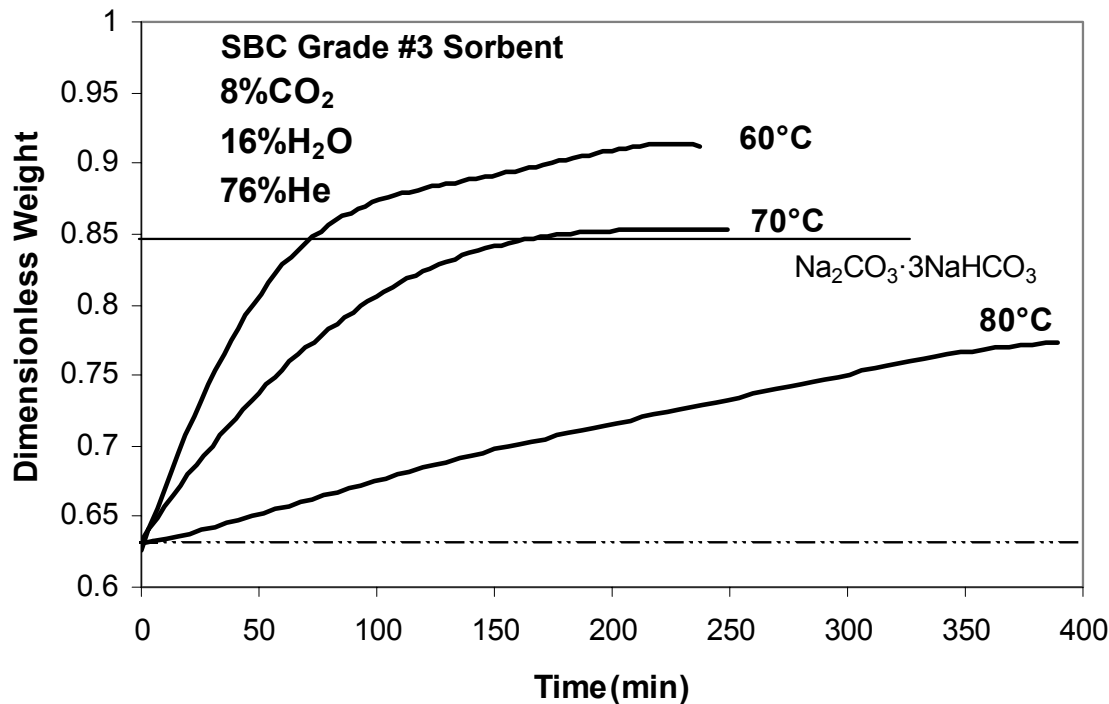
Sodium Carbonate Chemistry

Reaction	ΔH Kcal/gmol CO ₂
$2/3 \text{ Na}_2\text{CO}_3 \cdot 3\text{NaHCO}_3 \rightleftharpoons 5/3 \text{ Na}_2\text{CO}_3 + \text{CO}_2 + \text{H}_2\text{O}$	32.8
$5 \text{ NaHCO}_3 \rightleftharpoons \text{Na}_2\text{CO}_3 \cdot 3\text{NaHCO}_3 + \text{CO}_2 + \text{H}_2\text{O}$	32.1
$2\text{NaHCO}_3 \rightleftharpoons \text{Na}_2\text{CO}_3 + \text{CO}_2 + \text{H}_2\text{O}$	30.8

CO₂ removal is exothermic

Sorbent regeneration is endothermic

Fundamental Kinetic and Thermodynamic Studies



- First order reaction kinetics
 - CO₂
 - H₂O
- Temperature sensitive kinetics
 - NaHCO₃ product at 60 °C
 - Intermediate product (WS) at 70 °C
 - Higher temperatures decrease CO₂ removal
- Potential temperature control strategies
 - Cold diluents → solids
 - Liquid H₂O addition ($\Delta H_{\text{VAP}} = 10 \text{ Kcal/gmol}$)

Sorbent Operating Temperature Ranges

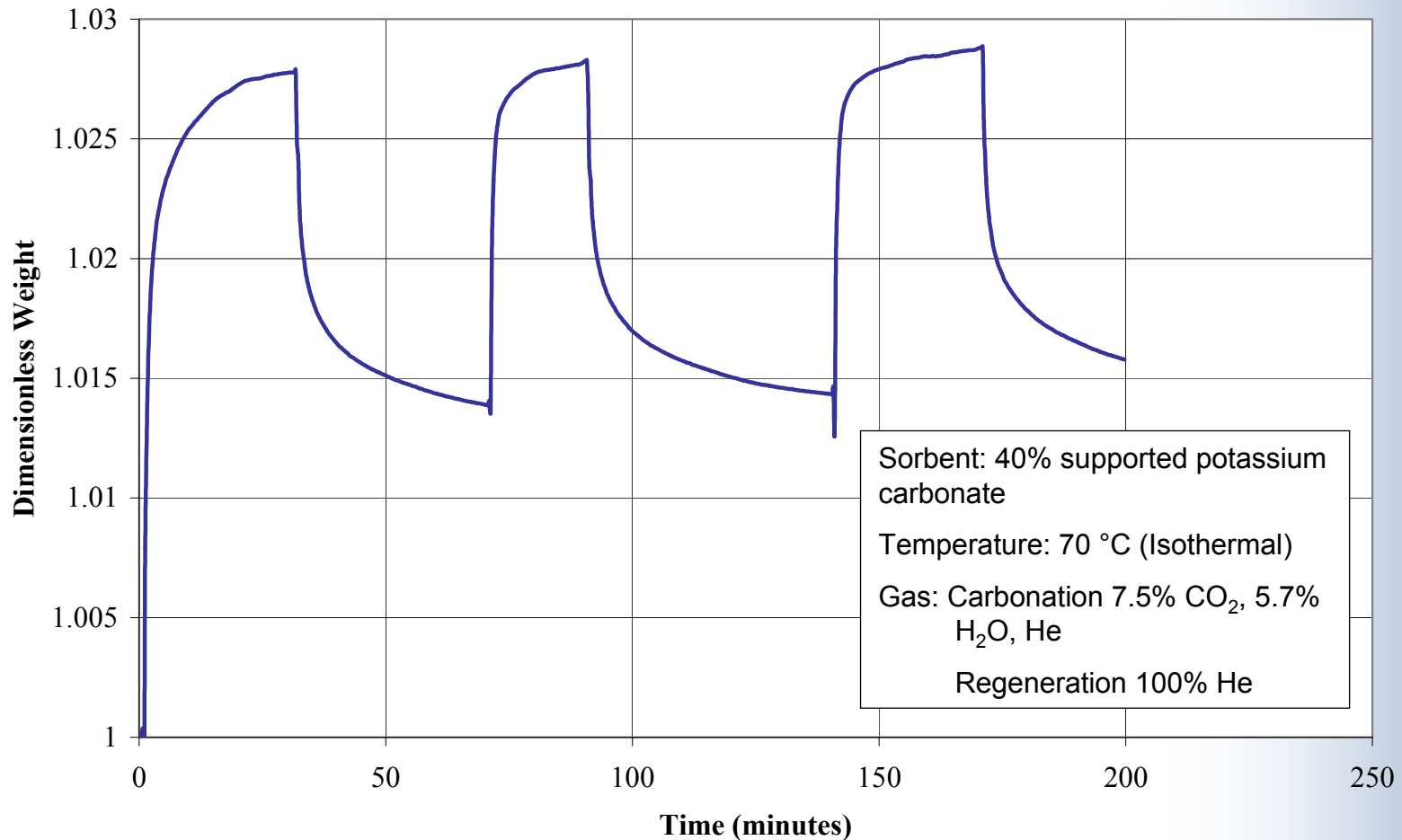
Sodium Carbonate

- Carbonation: 60 – 80 °C
- Regeneration (decarbonation; calcination): > 120 °C

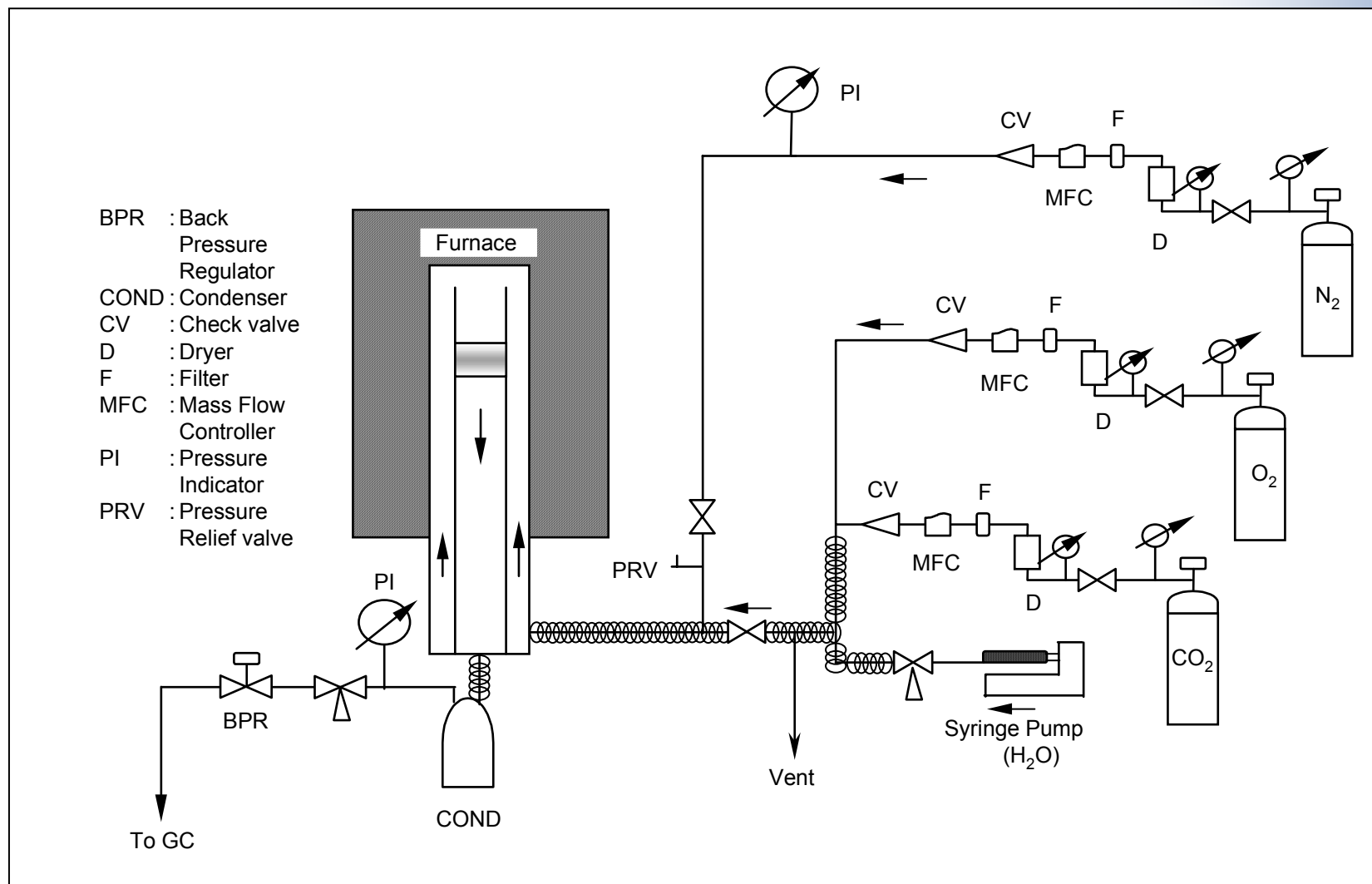
Potassium Carbonate

- Carbonation: up to 120 °C
- Regeneration (decarbonation; calcination): > 140 °C

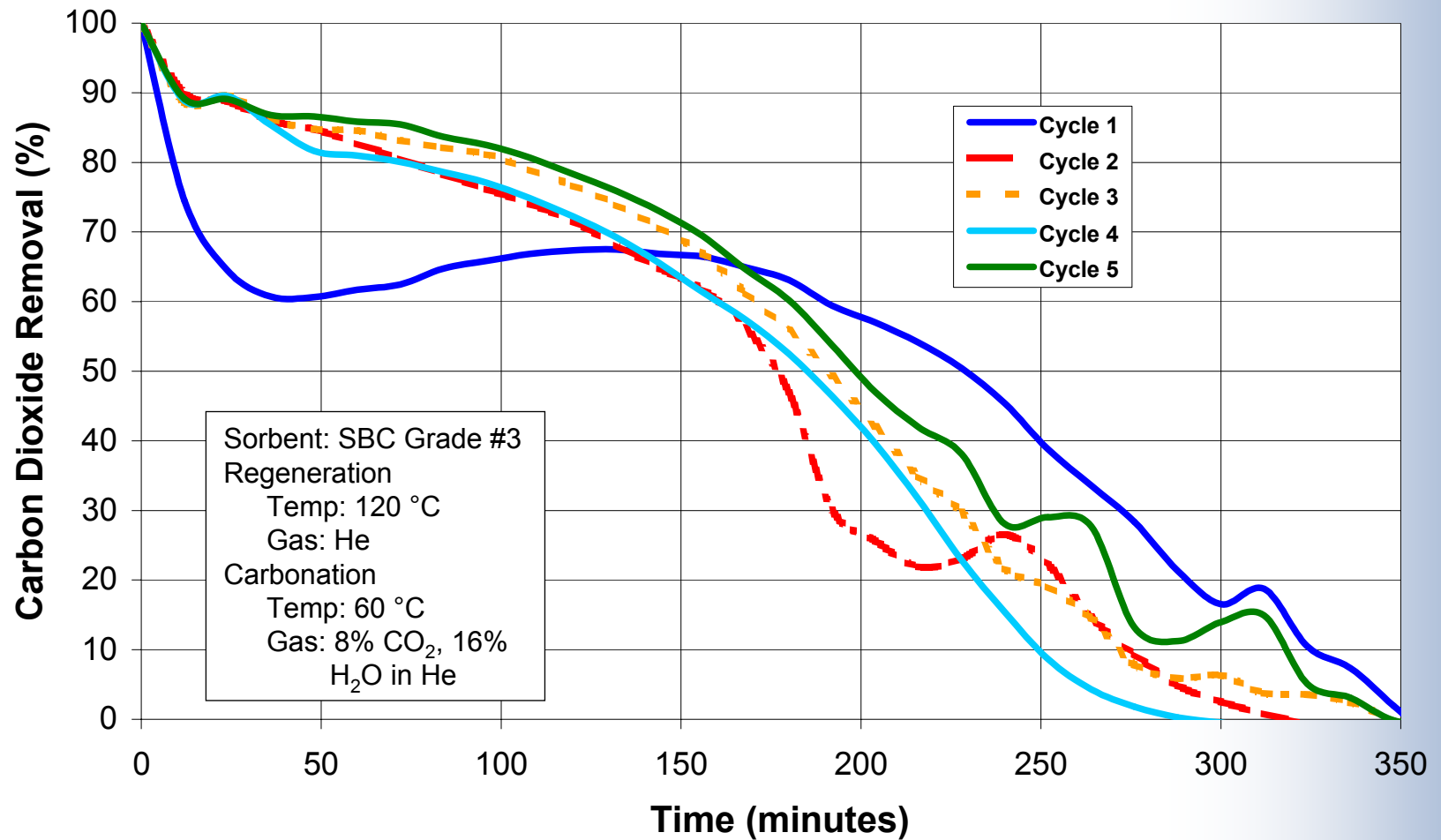
TGA Cyclic Reactivity Testing



Fixed-Bed Reactor System at LSU



Fixed-Bed Testing of SBC



SBC Sorbent Interaction with HCl and SO₂

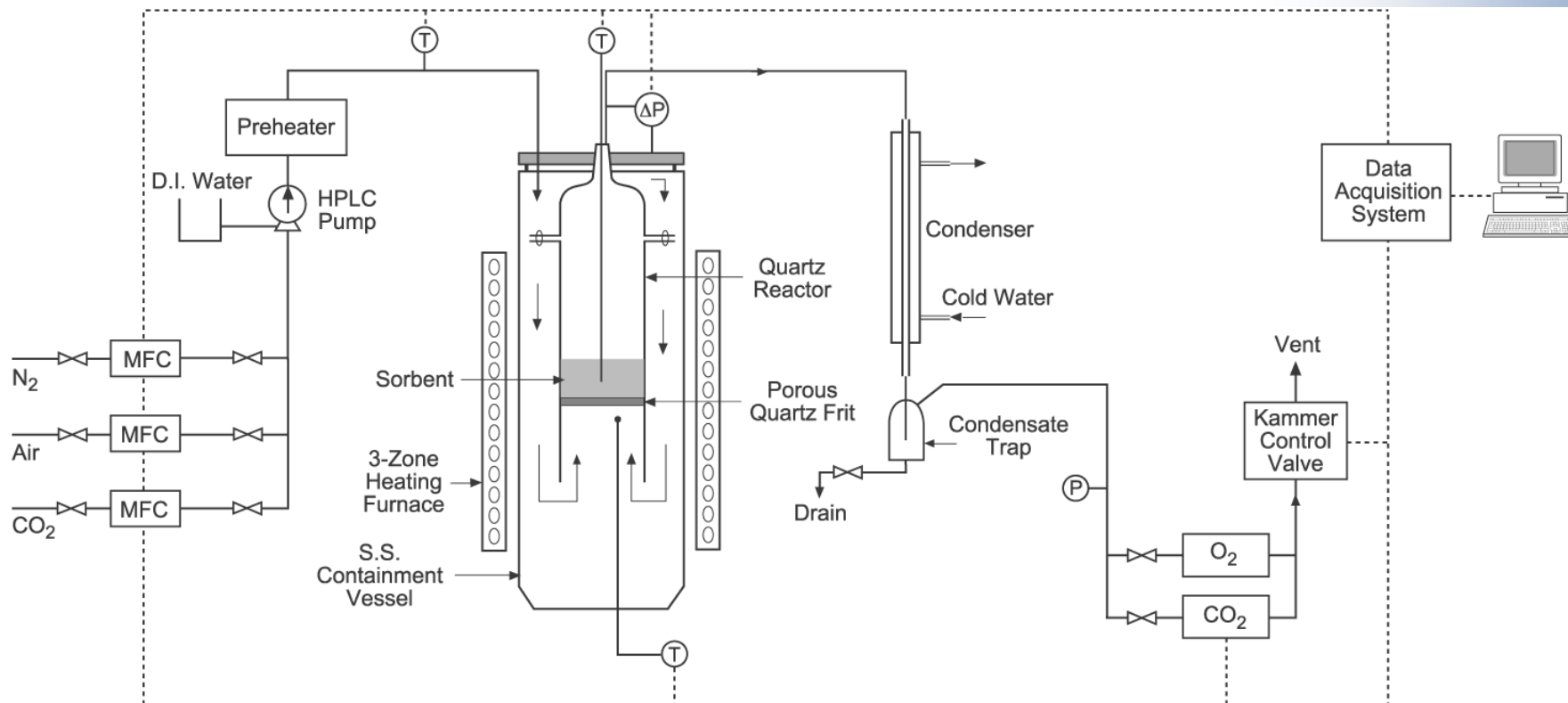
Hydrogen Chloride

- 1-inch Fluidized-bed testing
- 100 ppm HCl in simulated flue gas
- >98% removal with 1.2 sec superficial residence time

Sulfur Dioxide

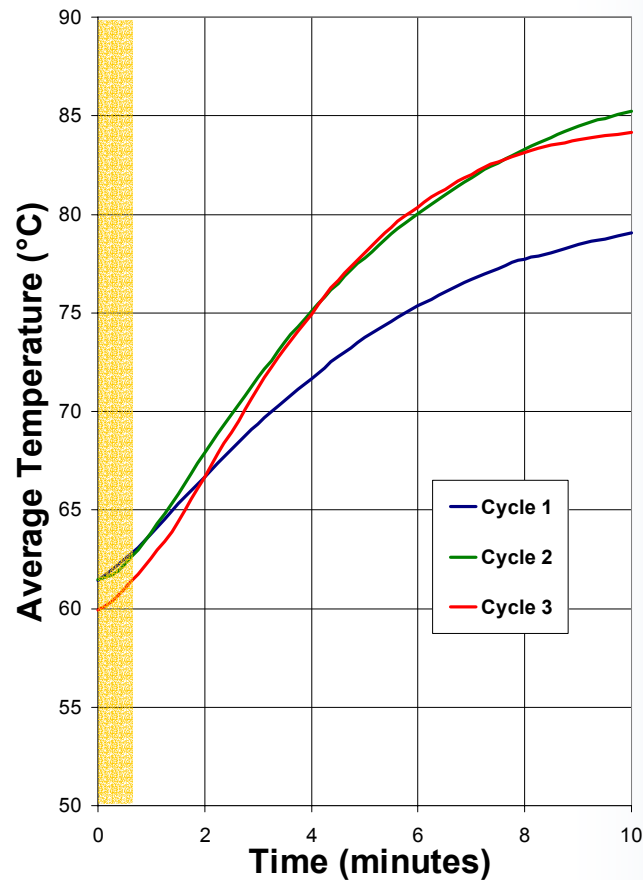
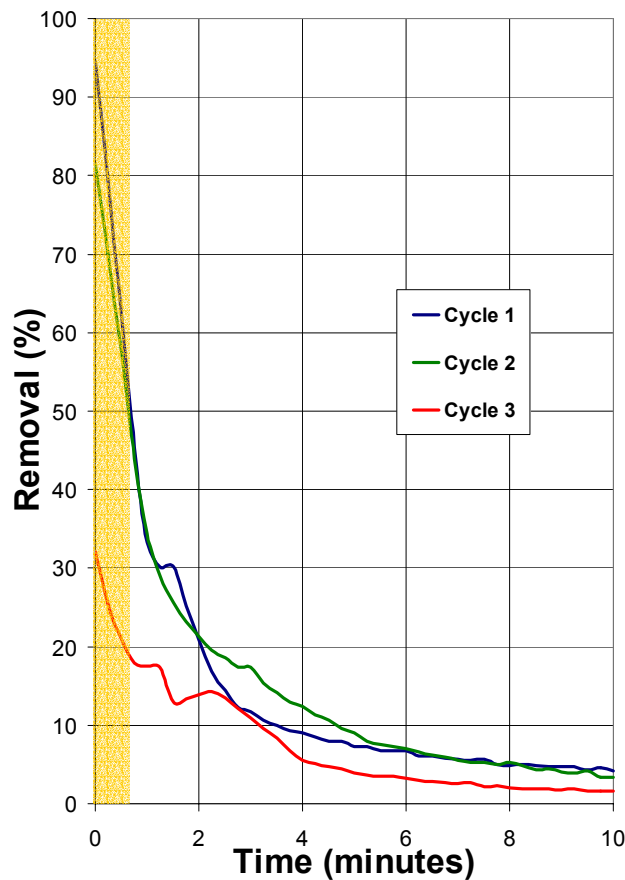
- TGA tests and 1-inch fluidized-bed testing
- 1000 ppm SO₂ in simulated flue gas
- >95% removal
- Irreversible at temperatures ≤ 200 °C

RTI's Bench-Scale Fluid-Bed Test Unit

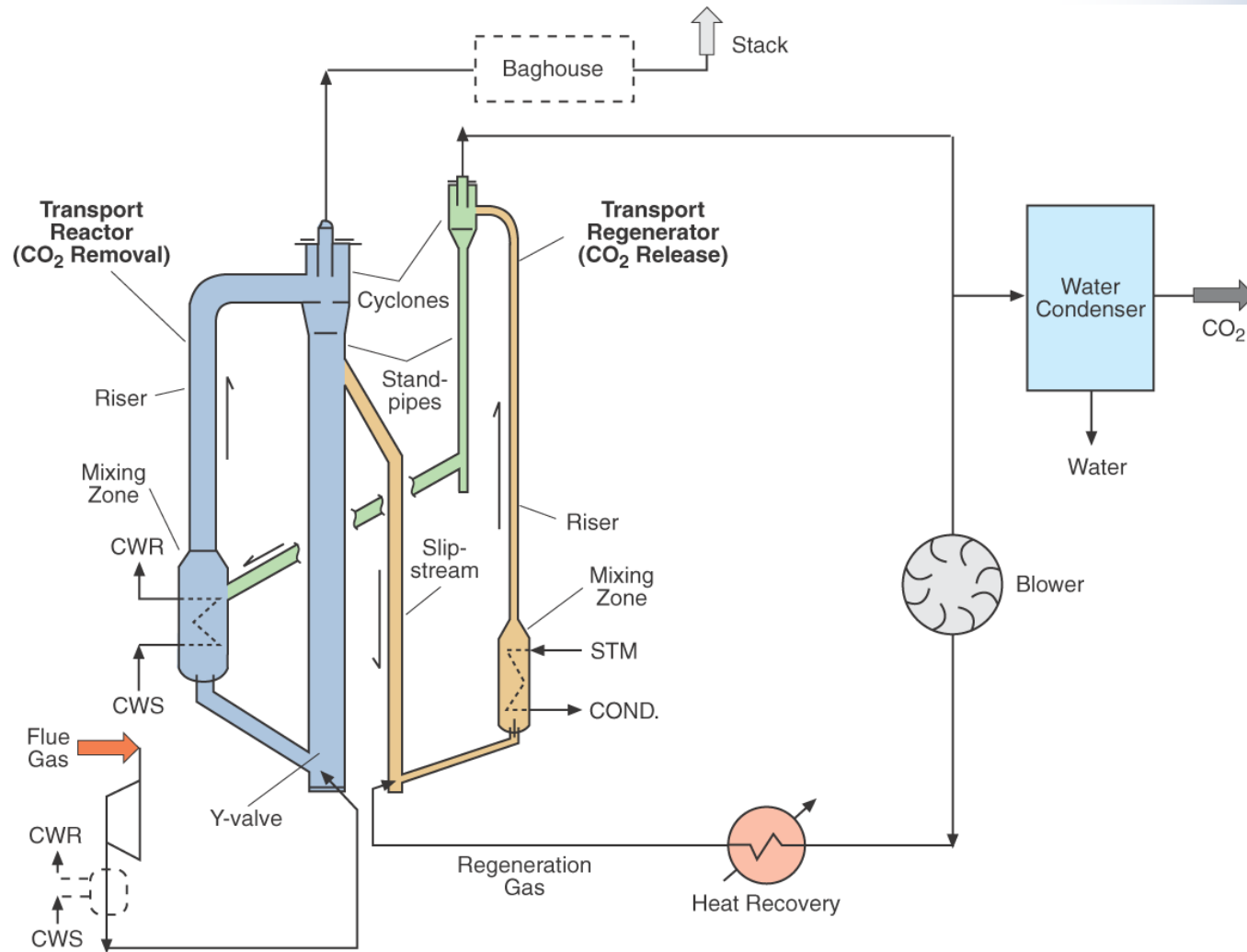


Fluid-Bed Testing of 40% Supported Sodium Carbonate

Carbonation in 7% Carbon Dioxide, 6% Water Vapor



Conceptual Transport Reactor System



Transport Reactor Approach

Advantages

- Low pressure drop (<1 psi [< 30 in. W.C.])
- Reliable and effective solid sorbent movement
- Superior temperature control

Sorbent design challenges

- High sorbent reactivity required
 - Short residence times (2-6 seconds)
- Highly attrition-resistant sorbent required
 - High sorbent flux rate

Engineering Design Challenges

Heat integration

- Capturing low-grade, low-value heat in the steam cycle for sorbent regeneration
- Minimizing parasitic power consumption
- Heat transfer:
 - Removal of carbonation heat of reaction
 - Addition of regeneration energy

Low pressure drop of flue gas stream

- Minimizing additional power requirements of the I.D. fan

Sorbent Transfer

- Efficiently move sorbent between carbonation reactor and regenerator

Heat Integration Analysis

Goal: Minimize process energy requirements

Target: Regeneration

- Largest energy requirement
- Low-level heat (120-140 °C)

Solutions

- Steam usage
- Low-level heat sources
 - Recover flue gas heat
 - Extract heat from cooling water
 - Alternative air preheating schemes

Comparison of Coal Fired Power Plants With and Without CO₂ Removal

Case	Heat Require- ment for CO ₂ Sor- bent Regeneration, Btu/lbmol CO ₂	Gross Plant Power kWe	Auxiliary Power Requirement kWe	Net Plant Power kWe	Plant Efficiency (HHV) %
EPRI Base Case 7C Coal Fired Steam Plant; no CO ₂ Removal	Not Applicable	491,108	29,050	462,058	40.5
EPRI Case 7A MEA CO ₂ Removal	71,140 ^E	402,254	72,730	329,524	28.9
EPRI Case 7A Re-calc'd	103,400 ^A	362,178	72,730	289,448	25.4
Comparison Case Na ₂ CO ₃ -based Dry CO ₂ Removal	60,000	416,144	72,730	343,414	30.1
90% CO ₂ Removal for Applicable Cases For all cases: Heat input = 1,140,155 kW _{heat} (HHV) ^E EPRI, Evaluation of Innovative Fossil Fuel Power Plants with CO ₂ Removal, 2000 ^A Alstom Power, Engineering Feasibility and Economics of CO ₂ Capture on an Existing Coal-Fired Power Plant, 2001					

Summary of Research Findings

The sodium and potassium carbonate sorbents react readily to remove CO₂

The materials can be cycled repeatedly without appreciable loss of activity

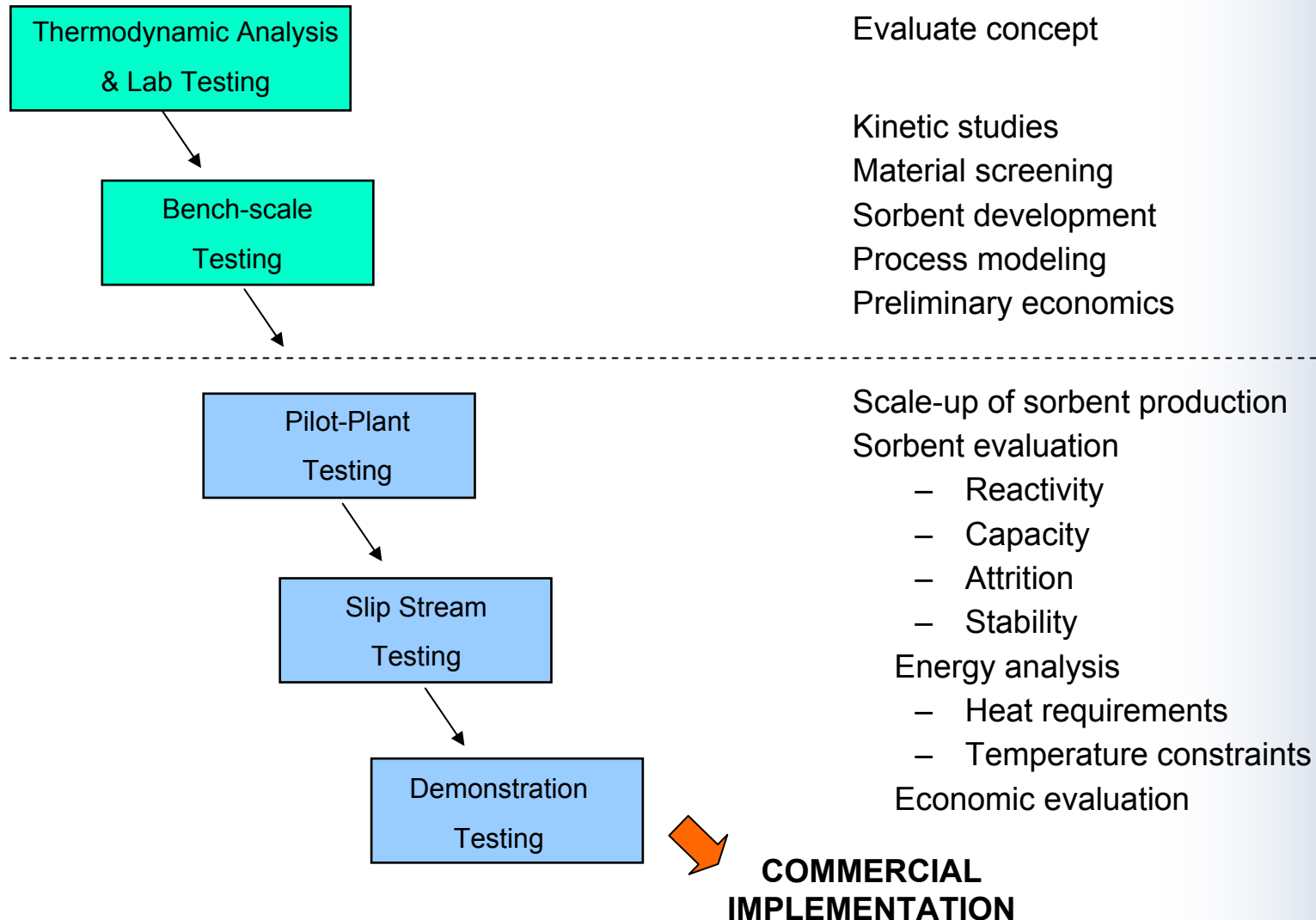
The carbonate/carbon dioxide reaction may be limited by considerations of heat removal from the sorbent particle

The high initial rates of reaction may be suitable for short residence time transport reactor systems

Regeneration of sorbent can be carried out in an essentially pure carbon dioxide stream

Supported materials provide suitable activity and attrition resistance

Technology Development Plan



Acknowledgements

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